

Lect 13 Rigid body (I) - fixed axis rotation

{ Rigid body

{ Rotation around a fixed axis

{ Moment of inertia

{ equation of motion of fixed axis rotation

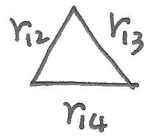
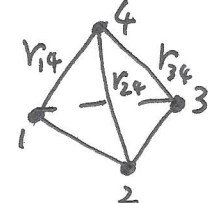
{ What's rigid body?



No elasticity!  
 The distance between any two points is fixed during the motion, i.e. no shape deformation.

how many degrees of freedom to describe a rigid body motion?

let's check

# of particles	# of degrees of freedom	if all distances fixed
1	3	•
2	$2 \times 3 - 1 = 5$	$r_{12}$
3	$3 \times 3 - 3 = 6$	
4	continuous no extra degrees of freedom (please prove!)	
5	6	
⋮	⋮	
N	6	

3 translational degrees of freedom

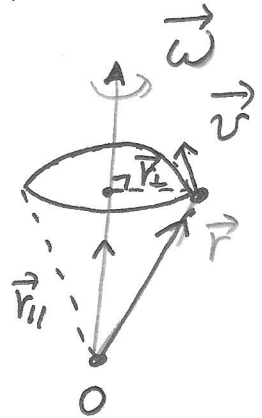
3 rotational degrees of freedom

§ Laws of rotation around a fixed axis.

instantaneous velocity at a point  $\vec{v} = \vec{v}_{\parallel} + \vec{v}_{\perp}$

$\vec{v}_{\parallel}$  is the component parallel to the rotation axis.

$\vec{v}_{\perp}$  is the component perpendicular to the axis



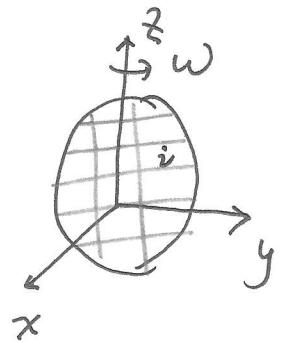
$$\vec{v} = \vec{\omega} \times \vec{r}_{\perp} = \vec{\omega} \times (\vec{r}_{\perp} + \vec{r}_{\parallel}) = \vec{\omega} \times \vec{r}$$

The angular momentum

$$\vec{L} = \sum_{i=1}^N \vec{l}_i = \sum_{i=1}^N m_i \vec{r}_i \times \vec{v}_i$$

$$\vec{v}_i = \vec{\omega} \times \vec{r}_i$$

$$\Rightarrow \vec{L} = \sum_{i=1}^N m_i \vec{r}_i \times (\vec{\omega} \times \vec{r}_i)$$



in our case  $\vec{\omega} = \omega \hat{z}$ ,  $\vec{r}_i = x_i \hat{x} + y_i \hat{y} + z_i \hat{z}$

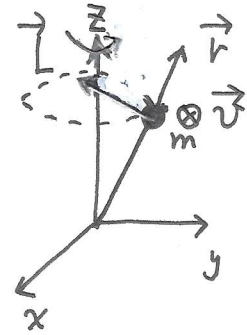
$$\begin{aligned} \vec{r}_i \times (\vec{\omega} \times \vec{r}_i) &= \vec{\omega} r_i^2 - \vec{r}_i (\vec{\omega} \cdot \vec{r}_i) \\ &= (x_i^2 + y_i^2 + z_i^2) \omega \hat{z} - \omega (z_i x_i \hat{x} + z_i y_i \hat{y} + z_i^2 \hat{z}) \\ &= -\omega z_i x_i \hat{x} - \omega z_i y_i \hat{y} + \omega (x_i^2 + y_i^2) \hat{z} \end{aligned}$$

$$L_z = \sum_{i=1}^N m_i \omega (x_i^2 + y_i^2) = I_z \omega, \text{ where } I_z = \sum_{i=1}^N m_i (x_i^2 + y_i^2)$$

$$\longrightarrow \int dx dy dz \rho (x^2 + y^2) = I_z \longleftarrow \text{moment of inertia}$$

$$\begin{aligned}
 L_x &= -\left(\sum_i m_i x_i z_i\right) \omega = I_{xz} \omega \neq 0 \\
 L_y &= -\left(\sum_i m_i y_i z_i\right) \omega = I_{yz} \omega \neq 0
 \end{aligned}
 \left. \vphantom{\begin{aligned} L_x \\ L_y \end{aligned}} \right\} \text{in general.}$$

**E**xample: If the mass distribution is unsymmetric with respect to the rotation axis,  $\vec{L} \neq \vec{\omega}$ .



### § Kinetic energy

$$E_k = \frac{1}{2} \sum_i m_i v_i^2 = \frac{1}{2} \sum_i m_i \omega^2 (x_i^2 + y_i^2) = \frac{I_z}{2} \omega^2$$

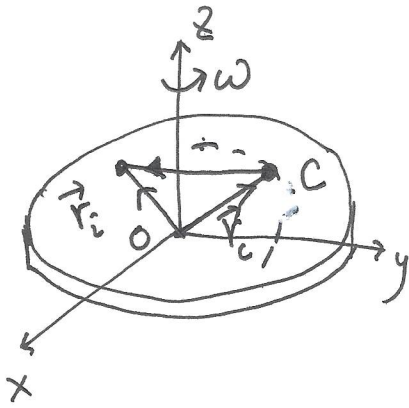
$$\vec{v} = -\omega y_i \hat{x} + \omega x_i \hat{y}$$

Parallel axis theorem:

If the rotation axis does not pass the center of mass, denote the distance between the mass center and the rotation axis as  $r_c$ ,

then  $I_z = I_{cz} + M r_c^2$ , where  $I_{cz}$  is the moment of inertia

if the rotation axis passes the center of mass.



$\vec{r}_i = \vec{r}_C + \vec{r}_i'$       $\vec{r}_i'$  is the displacement of "ith point" relative to C

$$I_z = \sum m_i r_i^2$$

$$= \sum_i m_i |\vec{r}_C + \vec{r}_i'|^2 = \sum_i m_i (r_C^2 + r_i'^2 + 2\vec{r}_C \cdot \vec{r}_i')$$

$$= M r_C^2 + I_{Cz} + 2\vec{r}_C \cdot \sum_i m_i \vec{r}_i'$$

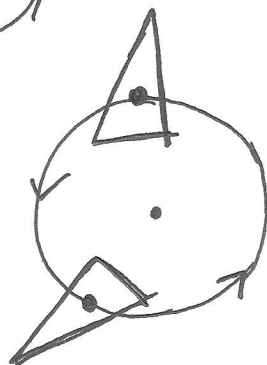
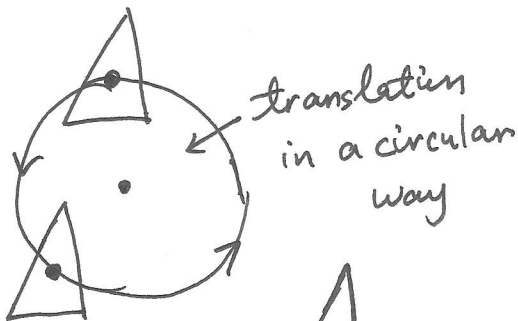
by definition  $\sum_i m_i \vec{r}_i = (\sum_i m_i) \vec{r}_C \Rightarrow \sum_i m_i \vec{r}_i' = 0$ .

Hence  $I_z = I_{Cz} + M r_C^2$ .

Then 
$$E_K = \frac{1}{2} I_z \omega^2 = \frac{1}{2} I_{Cz} \omega^2 + \frac{1}{2} M (r_C \omega)^2$$

Kinetic energy of a rotating slab = kinetic energy in the center of mass frame

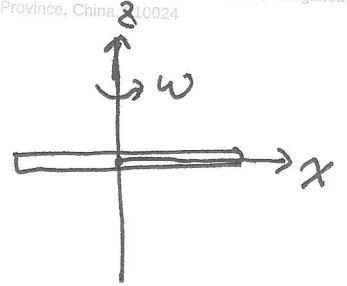
+ the translation energy as a whole object



rotation around an axis away from the center of mass.

## ★ examples of moment of inertial

- ① Uniform thin rod - rotation axis passes center of mass

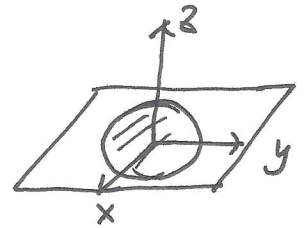


$$I_z = \int_{-\frac{L}{2}}^{\frac{L}{2}} dx \rho x^2 = \frac{\rho}{3} x^3 \Big|_{-\frac{L}{2}}^{\frac{L}{2}} = \frac{\rho}{12} L^3 = \frac{(\rho L) L^2}{12} = \frac{M}{12} L^2$$

if the rotation axis is located at one end, then

$$I_z = I_{cm} + M \left(\frac{L}{2}\right)^2 = \frac{M}{3} L^2$$

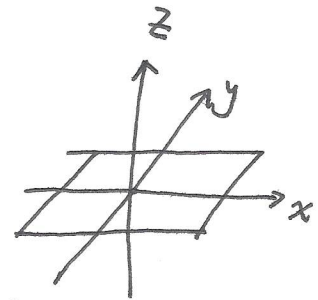
- ② Circular disk - rotation axis passes its center



$$I_z = \int dx \int dy \rho (x^2 + y^2) = \rho \int_0^R r dr \int_0^{2\pi} d\theta r^2 = 2\pi \rho \cdot \frac{R^3}{4}$$

$$= (\pi R^2 \rho) \frac{R^2}{2} = \frac{1}{2} MR^2$$

- ③ rectangular plate - axis passing the center

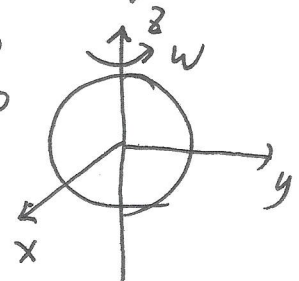


$$I_z = \int_{-\frac{a}{2}}^{\frac{a}{2}} dx \int_{-\frac{b}{2}}^{\frac{b}{2}} dy \rho (x^2 + y^2) = \rho \left( b \frac{x^3}{3} \Big|_{-\frac{a}{2}}^{\frac{a}{2}} + a \cdot \frac{y^3}{3} \Big|_{-\frac{b}{2}}^{\frac{b}{2}} \right)$$

$$= \rho \left( \frac{ba^3}{12} + \frac{ab^3}{12} \right) = \frac{\rho ab}{12} (a^2 + b^2) = \frac{M}{12} (a^2 + b^2)$$

- ④ uniform solid sphere

$$\begin{cases} x = r \sin \theta \cos \phi \\ y = r \sin \theta \sin \phi \end{cases}$$



$$I = \int r^2 dr \sin \theta d\theta d\phi \rho (r^2 \sin^2 \theta)$$

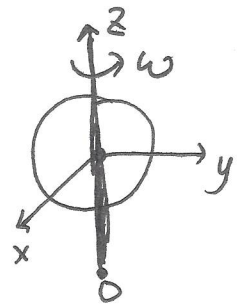
$$= \rho \int_0^R r^4 dr \int_0^\pi \sin^3 \theta d\theta \int_0^{2\pi} d\phi$$

$$\int_0^\pi \sin^2 \theta d\theta = -\int_0^\pi \sin^2 \theta d \cos \theta = + \int_{-1}^1 (1-x^2) dx = x - \frac{x^3}{3} \Big|_{-1}^1 = \frac{4}{3}$$

$$\Rightarrow I = \rho \cdot \frac{R^5}{5} \cdot \frac{4}{3} \cdot 2\pi = \left(\frac{4\pi}{3} R^3 \rho\right) \frac{2}{5} R^2 = \frac{2}{5} MR^2$$

§: Equation of motion for fixed axis rotation

Set  $\vec{\omega}$  is along the  $\hat{z}$ -axis, for fixed axis rotation



$$L_z = I_z \omega,$$

$$\frac{dL_z}{dt} = \tau_z \leftarrow \text{torque}$$

Actually, we can pick up any point O at the rotation axis as the origin. We proved before

$$\frac{d}{dt} \vec{L} = \sum_{i=1}^N \vec{r}_i \times \vec{F}_i^{ex}$$

we take the z-component; ①  $L_z = I_z \omega$  and  $I_z = \int dx dy dz \rho(x^2+y^2)$

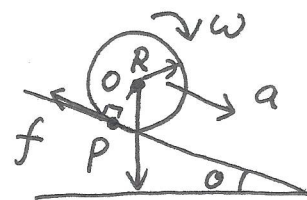
i.e.  $L_z$  does not depend on the location of "O" on the axis.

②  $(\vec{r}_i \times \vec{F}_i^{ex})_z = x_i F_i^y - y_i F_i^x$ , which does not depend on the z-location of "O" either. Hence, we have

$$\frac{dL_z}{dt} = \tau_z$$

define for the rotation axis, independent of the location of "O" along the axis

Example: rolling without slipping



① Constraint:  $\vec{v}_P = \vec{v}_O + \vec{\omega} \times \vec{r}_{Op} = 0$

$\Rightarrow v_O = \omega R \Rightarrow a = R \frac{d\omega}{dt}$

with respect  
to center  
of Mass.

$f \cdot R = I \frac{d\omega}{dt}$

$Mg \sin\theta - f = Ma$

$\Rightarrow Mg \sin\theta - I \frac{d\omega}{dt} \cdot \frac{1}{R} = Ma$

$Mg \sin\theta = \left( \frac{I}{R^2} + M \right) a$

$\Rightarrow a = \frac{1}{1 + I/MR^2} g \sin\theta$

② energy conservation

$Mg h = \frac{1}{2} M v^2 + \frac{1}{2} I \omega^2 = \frac{1}{2} M v^2 + \frac{1}{2} I \left( \frac{v}{R} \right)^2$

$\Rightarrow g \frac{dh}{dt} = v \frac{dv}{dt} \left( 1 + \frac{I}{MR^2} \right)$

$\frac{dh}{dt} = v \sin\theta, a = \frac{dv}{dt} \Rightarrow a = \frac{g \sin\theta}{1 + I/MR^2}$

comment: ①  $f < Mg \cos\theta \cdot \mu$ , hence,  $\mu$  cannot be too small to achieve roll without slipping.

② the largest angle for rolling without slipping

$g \sin\theta \left( 1 - \frac{1}{1 + I/MR^2} \right) < g \cos\theta \cdot \mu \Rightarrow \tan\theta < \frac{\mu (1 + I/MR^2)}{I/MR^2}$

$\tan\theta \leq \mu \left( \frac{MR^2}{I} + 1 \right)$



$\tan\theta < \frac{\mu (1 + I/MR^2)}{I/MR^2}$



Example: A cylinder is put on a rug.

Pull the rug with an acceleration  $\vec{a}$ ,  
and the cylinder ~~is~~ does not slip.

Then describe the motion of the cylinder.

\* We use the non-inertial frame of the rug.

Then in this frame, there's the inertial force

$$\vec{F}_{\text{inert}} = M a \hat{x}$$

The torque:  $\frac{dw}{dt} = \frac{a'}{R} = \frac{f \cdot R}{I}$

and  $\vec{F} + \vec{f} = M \vec{a}'$

$$\Rightarrow M a' = M a - \frac{I a'}{R^2}$$

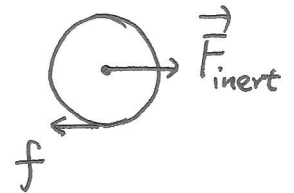
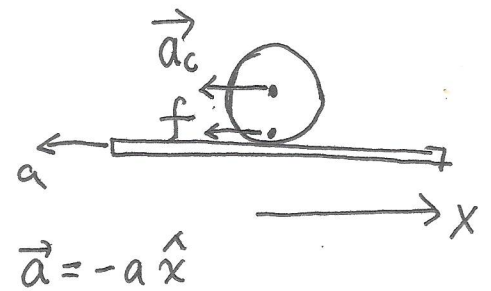
$$\Rightarrow a' = \frac{M}{M + I/R^2} a = \frac{1}{1 + \frac{I}{MR^2}} a = \frac{2}{3} a \quad \text{if } I = \frac{1}{2} MR^2$$

The rug acceleration  $\vec{a} = -a \hat{x} \Rightarrow$  the cylinder

$$\vec{a}_c = \vec{a} + \vec{a}' = -\frac{I/MR^2}{1 + I/MR^2} a \hat{x} = -\frac{I}{MR^2 + I} a \hat{x}$$

$$\Rightarrow I = \frac{1}{2} MR^2$$

$$\vec{a}_c = -\frac{a}{3} \hat{x}, \quad \text{and} \quad f = -\frac{M}{3} a \hat{x}$$



$a'$  is the acceleration  
 of the cylinder  
 center of mass w.r.t  
 in the rug frame.